

Name: Key

FO-2133 Forest Measurement  
Exam 2 - 2008

1. Height measurement:

You just checked your Suunto clinometer with the peg method and found the double-error between 2 trees was +8.8 ft at a distance of 110 ft.

- A. The percent error of the clinometer is computed (with sign) to be: +4% (5)

$$\% \text{ Error} = \left( \frac{+8.8}{110} \right) / 2 = +4\%$$

Using the percent scale, you measure the total height of one of the peg-method trees at the specified horizontal distance above; i.e 110 ft..

the reading at the top = +85 ft

the reading at the ground line = -5 ft

- B. The correct height of the tree is computed to be: 95 ft (10)

$$H = \left( 1 - .04 \right) \left( \frac{110}{100} \right) [85 - (-5)] = (0.96)(1.1)(90)$$

2. Volume computation:

Given: A single tree segment is 16.5 ft in length and has a butt diameter of 17.6 inches, o.b., with single bark thickness of 0.8 inches and a top diameter of 13.5 inches, o.b., with a single bark thickness of 0.5 inches.

- A. The cubic volume, outside bark, of the total log is: 22.14 cubic feet (5)

$$V_{ob}^3 = \left[ \frac{.005454 (17.6)^2 + 0.005454 (13.5)^2}{2} \right] 16.5$$

- B. The cubic volume, inside bark, of the total log is: 18.54 cubic feet (5)

$$V_{ib}^3 = \left[ .005454 \left[ \frac{16^2 + 12.5^2}{2} \right] \right] 16.5$$

- C. The scaling length of the log for Doyle board foot volume is: 16 feet (5)

- D. The scaling diameter of the log for Doyle board foot volume is: 13 inches (5)

- E. The Doyle Board Foot volume of the single log is: 81 bd. ft (5)

$$\text{Doyle} = \frac{(3-4)^2 \times 16}{16}$$

- F. The board foot per cubic foot (o.b.) ratio of the log is: 3.66 (5)

$$\text{Bd ft} : \text{ft}^3 = \frac{81}{22.14} = 3.66$$

Name: \_\_\_\_\_

3. Cruise volume and statistical computations:

Given the following tally from a 0.2 acre plot cruise on 40 acres, compute the volume estimates, precision statistics, and stand and stock table for the cruise.

Tree Equations:  $H = 120e^{\left(\frac{-4.15}{DBH}\right)}$

Bd. Ft Volume =  $10 + 0.01(D^2H)$

Plot#	DBH	#Trees							
1	10	1							
	12	2							
	14	3							
2	12	2							
	14	3							
	16	4							
3	10	3							
	14	2							
	16	2							
4	10	2							
	12	4							
	14	3							
	16	2							
		<b>Sum</b>							
		<b>Mean</b>							

s <sup>2</sup>		(5)
s		(5)
s_xbar		(5)
t		(5)
SE%		(5)
CV%		(5)

Stand & Stock Table

DBH		DBH	Trees/ac	Volume/ac	Total Trees	Total Volume	
10							
10							
10		10					(4)
12							
12							
12		12					(4)
14							
14							
14		14					(4)
16							
16							
16		16					(4)
		<b>Totals</b>					(4)

The best estimate of mean volume per acre is: \_\_\_\_\_ Bd. Ft. (5)

3. Cruise volume and statistical computations:

Given the following tally from a 0.2 acre plot cruise on ~~80~~<sup>40</sup> acres, compute the volume ~~and~~<sup>estimates</sup> precision statistics for the cruise. (and stand 15 foot table)

Tree Equations:  $H = 120e^{\left(\frac{-4.15}{DBH}\right)}$   
 $Volume = 10 + 0.01(D^2H)$

Plot#	DBH	Height	#Trees	PACF	Trees/ac	Vol/tree	Vol/ac	Plot Vol	Vol <sup>2</sup>
1	10	79	1	5	5	89	446	4542	20629284
	12	85	2	5	10	132	1323		
	14	89	3	5	15	185	2773		
2	12	85	2	5	10	132	1323	9036	81650123
	14	89	3	5	15	185	2773		
	16	93	4	5	20	247	4940		
3	10	79	3	5	15	89	1339	5657	32006201
	14	89	2	5	10	185	1849		
	16	93	2	5	10	247	2470		
4	10	79	2	5	10	89	892	8781	77107508
	12	85	4	5	20	132	2646		
	14	89	3	5	15	185	2773		
	16	93	2	5	10	247	2470		
				165	<b>Sum</b>	28016	28016	28016	211393116
				41.3	<b>Mean</b>	7004	7004	7004	

$s^2$  5054094  
 $s$  2248  
 $s_{\bar{x}}$  1113  
 $t$  3.1820  
 $SE\%$  51  
 $CV\%$  32

(5) 5056350  
 (5) 2248.63  
 (5) 1113.02  
 (5)  $\alpha = .05, n-1 = 3$   
 (5) 50.56 = 5.9%  
 (5) 32.10%  
 30

DBH	Trees/ac	Vol/ac	DBH	Trees/ac	Volume/ac	Total Trees	Total Volume
10	5	446					
10	15	1339					
10	10	892	10	7.5	669	300	26,772 (4)
12	10	1323					
12	10	1323					
12	20	2646	12	10.0	1,323	400	52,911 (4)
14	15	2773					
14	15	2773					
14	10	1849					
14	15	2773	14	13.8	2,542	550	101,675 (4)
16	20	4940					
16	10	2470					
16	10	2470	16	10.0	2,470	400	98,806 (4)
<b>Totals</b> 41.3						1,650	280,165 (4)

Best Estimate of Mean Volume per acre is: 7,004 Bd ft/ac (5)

## Equation Formula Sheet

$$s^2 = \frac{\left[ \sum_{i=1}^n x_i^2 - \frac{(\sum_{i=1}^n x_i)^2}{n} \right]}{(n-1)} \quad s^2 = \frac{\left[ \sum_{i=1}^n x_i^2 - \bar{x} \sum_{i=1}^n x_i \right]}{(n-1)} \quad s = \sqrt{s^2}$$

$$CV\% = \left( \frac{s}{\bar{x}} \right) (100)$$

$$s_{\bar{x}} = \sqrt{\frac{s^2}{n} \left( 1 - \frac{n}{N} \right)}$$

$$\bar{x} \pm (t_{\alpha, n-1}) s_{\bar{x}}$$

$$SE\% = \left( \frac{t_{\alpha, n-1} s_{\bar{x}}}{\bar{x}} \right) 100\%$$

$$SS_y: \sum y^2 = \sum Y^2 - \frac{(\sum Y)^2}{n}$$

$$b_1 = \frac{\sum xy}{\sum x^2} = \frac{SP_{xy}}{SS_x}$$

$$SS_x: \sum x^2 = \sum X^2 - \frac{(\sum X)^2}{n}$$

$$b_0 = \bar{Y} - b_1 \bar{X}$$

$$SP_{xy}: \sum xy = \sum XY - \frac{\sum X \sum Y}{n}$$

TSS  $SS_y = \sum y^2$

$$ESS = \sum (Y - \hat{Y})^2$$

RSS  $\frac{(SP_{xy})^2}{SS_x} = \frac{(\sum xy)^2}{\sum x^2} = b_1 \sum xy$

$$I^2 = \left( 1 - \frac{\text{Error SS}}{\text{Total SS}} \right)$$

$$S_{y.x} = \sqrt{\frac{\sum (Y - \hat{Y})^2}{n-2}} = \sqrt{\frac{ESS}{n-2}}$$

$$S_{y.x} = \sqrt{\frac{\sum y_i^2 - b_1 \sum xy}{n-2}} = \sqrt{\frac{ESS}{n-2}}$$

$$\text{height} = \left( 1 - \frac{\% \text{ error}}{100} \right) \left[ \frac{\text{horizontal distance}}{\text{index distance}} \right] (\text{Reading@top} - \text{Reading@bottom})$$

Smalian:  $ft^3 = [(B + b)/2] L$

Huber:  $ft^3 = [(B_{1/2})] L$

Newton:  $ft^3 = [(B + 4 B_{1/2} + b)/6] L$

Doyle Board Feet =  $(D - 4)^2 L / 16$

Scribner Board Feet =  $(0.79D^3 - 2D - 4) L / 16$

International 1/4 Board Feet  $4 \text{ ft. log} = 0.199D^2 - 0.6420D$

$8 \text{ ft. log} = 0.597D^2 - 1.3290D - 0.7143$

$16 \text{ ft. log} = 0.796D^2 - 1.3740D - 1.2295$

## Student's t-Table

### The Distribution of t

df	Probability = $\alpha$								
	0.5	0.4	0.3	0.2	0.1	0.05	0.02	0.01	0.001
1	1.000	1.376	1.963	3.078	6.314	12.706	31.821	63.657	636.619
2	0.819	1.061	1.386	1.886	2.920	4.303	6.965	9.925	31.598
3	0.765	0.978	1.250	1.638	2.353	3.182	4.541	5.841	12.941
4	0.741	0.941	1.190	1.533	2.132	2.776	3.747	4.604	8.610
5	0.727	0.920	1.156	1.476	2.015	2.571	3.365	4.032	6.856
6	0.718	0.906	1.134	1.440	1.943	2.447	3.143	3.707	5.959
7	0.711	0.896	1.119	1.415	1.895	2.365	2.998	3.499	5.405
8	0.706	0.889	1.108	1.397	1.860	2.306	2.896	3.355	5.041
9	0.703	0.883	1.100	1.383	1.833	2.262	2.821	3.250	4.781
10	0.700	0.879	1.093	1.372	1.812	2.228	2.764	3.169	4.587
11	0.697	0.876	1.088	1.363	1.769	2.201	2.718	3.106	4.437
12	0.695	0.873	1.083	1.356	1.782	2.179	2.681	3.055	4.318
13	0.694	0.870	1.079	1.350	1.771	2.160	2.650	3.012	4.221
14	0.692	0.868	1.076	1.345	1.761	2.145	2.624	2.977	4.140
15	0.691	0.866	1.074	1.341	1.753	2.131	2.602	2.947	4.073
16	0.690	0.865	1.071	1.337	1.746	2.120	2.583	2.921	4.015
17	0.689	0.863	1.069	1.333	1.740	2.110	2.567	2.898	3.965
18	0.688	0.862	1.067	1.330	1.734	2.101	2.552	2.878	3.922
19	0.688	0.861	1.066	1.328	1.729	2.093	2.539	2.861	3.883
20	0.687	0.860	1.064	1.325	1.725	2.086	2.528	2.845	3.850
21	0.686	0.859	1.063	1.323	1.721	2.080	2.518	2.831	3.819
22	0.686	0.858	1.061	1.321	1.717	2.074	2.508	2.819	3.792
23	0.685	0.858	1.060	1.319	1.714	2.069	2.500	2.807	3.767
24	0.685	0.857	1.059	1.318	1.711	2.064	2.492	2.797	3.745
25	0.684	0.856	1.058	1.316	1.708	2.060	2.485	2.787	3.725
26	0.684	0.856	1.058	1.315	1.706	2.056	2.479	2.779	3.707
27	0.684	0.855	1.057	1.314	1.703	2.052	2.473	2.771	3.690
28	0.683	0.855	1.056	1.313	1.701	2.048	2.467	2.763	3.674
29	0.683	0.854	1.055	1.311	1.699	2.045	2.462	2.756	3.659
30	0.683	0.854	1.055	1.310	1.697	2.042	2.457	2.750	3.646
40	0.681	0.851	1.050	1.303	1.684	2.021	2.423	2.704	3.551
60	0.679	0.848	1.046	1.296	1.671	2.000	2.390	2.660	3.460
120	0.677	0.845	1.041	1.289	1.658	1.980	2.358	2.617	3.373
$\infty$	0.674	0.842	1.036	1.282	1.645	1.960	2.326	2.576	3.291